A Double-Sided LCC Compensation Network and Its Tuning Method for Wireless Power Transfer

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Abstract—This paper proposes a double-sided LCC compensation network and its tuning method for wireless power transfer (WPT). With the proposed topology and its tuning method, the resonant frequency is irrelevant with the coupling coefficient between the two coils and is also independent of the load condition, which means that the system can work at a constant switching frequency. Analysis in frequency domain is given to show the characteristics of the proposed method. We also propose a method to tune the network to realize zero voltage switching (ZVS) for the Primary-side switches. Simulation and experimental results verified analysis and validation of the proposed compensation network and the tuning method. A wireless charging system with output power of up to 7.7 kW for electric vehicles was built, and 96% efficiency from dc power source to battery load is achieved.

Index Terms—Battery charger, current source, electric vehicle, wireless power transfer (WPT), zero voltage switching (ZVS).

NOMENCLATURE

- \( S_1 \sim S_4 \): Primary-side MOSFETs.
- \( D_1 \sim D_4 \): Secondary-side rectifier diodes.
- \( L_1 \): Self-inductance of the transmitting coil.
- \( L_{c1} \): Primary-side compensation inductance.
- \( L_2 \): Self-inductance of the receiving coil.
- \( L_{c2} \): Secondary-side compensation inductance.
- \( L_{s1} \): Leakage inductance of the transmitting coil.
- \( L_{s2} \): Leakage inductance of the receiving coil.
- \( L_m \): Magnetizing inductance referred to the primary side.
- \( L'_{c1} \): Converted secondary-side compensation inductance referred to the primary side.
- \( L'_{c2} \): Equivalent inductance of the primary-side series capacitor and leakage inductance.
- \( L'_{e1} \): Converted equivalent inductance of the secondary-side series capacitor and leakage inductance referred to the primary side.
- \( \Delta L_{c2} \): Decrement of the equivalent inductance of secondary-side series capacitor and leakage inductance.
- \( \Delta L'_{c2} \): Converted decrement of the equivalent inductance of the secondary-side series capacitor and leakage inductance referred to the primary side.
- \( C_1 \): Primary-side series compensation capacitor.
- \( C_{f1} \): Primary-side parallel compensation capacitor.
- \( C_2 \): Secondary-side series compensation capacitor.
- \( C_{f2} \): Secondary-side parallel compensation capacitor.
- \( C'_{f2} \): Converted secondary-side series compensation capacitor referred to the primary side.
- \( C'_{c2} \): Converted secondary-side parallel compensation capacitor referred to the primary side.
- \( \Delta C_2 \): Increment of the secondary-side series compensation capacitor.
- \( M \): Mutual inductance between the transmitting and receiving coils.
- \( k \): Coupling coefficient between the transmitting and receiving coils.
- \( n \): Equivalent turns ratio between the transmitting and receiving coils.
- \( \omega_0 \): Resonant angular frequency.
- \( U_{AB} \): Phasor of the first-order input voltage applied on the primary side.
- \( U_{AB_{mth}} \): First-order rms value of the input voltage.
- \( u_{ab} \): Phasor of the \( m \)th-order input voltage.
- \( U_{ab} \): The square-wave output voltage of the secondary side before the rectifier.
- \( U_{ab_{min}} \): Phasor of the first-order output voltage before the rectifier.
- \( U_{ab} \): First-order rms value of the output voltage before the rectifier.
- \( U_{r} \): Minimum rms value of the output voltage before the rectifier.
- \( U_{r_{min}} \): Phasor of the first-order output voltage referred to the primary side.

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different compensation topologies have been proposed and implemented to tune the two coils working at a resonant frequency in a wide range of applications. There are four basic topologies depending on how the compensation capacitors are added to the transmitting and receiving coils, namely, series-series (SS), series-parallel, parallel-series, and parallel-parallel topologies [9], [10]. Some other novel topologies have also been proposed in the literature. In [11], a dual topology is realized by switching between a parallel-compensated secondary side and a series-compensated secondary side to realize both constant current mode and constant voltage mode. Moreover, the transmitting and receiving coils need to be connected to the power electronics converters. To achieve high efficiency for the complete WPT system, some other superior topologies have been proposed. In [12], an LCL converter is formed by adding LC compensation network between the converter and the transmitting coil. There are two advantages for the LCL converter when the system works at the resonant frequency. First, the inverter only supplies the active power required by the load; second, the current in the primary-side coil is independent of the load condition. In [13], an LC compensation network at both primary and secondary sides is proposed for bidirectional power transfer. The design of an LCL converter usually requires the same value for the two inductors. To reduce the additional inductor size and cost, usually, a capacitor is put in series with the primary-side coil, which forms an LCC compensation network. By utilizing an LCC compensation network, a zero current switching (ZCS) condition could be achieved by tuning the compensation network parameters [14]. Moreover, when the LCC compensation network is adopted at the secondary side, the reactive power at the secondary side could be compensated to form a unit power factor pickup [15].

One of the uniqueness of WPT systems is the high spatial freedom of the coils. This means the air-gap variation and misalignment of the transmitting and receiving coils are inevitable. Usually, the system parameters and resonant frequency of the primary and secondary resonant tanks change when the coupling condition changes [16]. With traditional compensation topologies, to achieve high efficiency, a tuning method is needed to maintain the resonance when the air gap changes or misalignment happens. There are two main methods, namely, frequency control [17], [18] and impedance matching [19], [20]. In [18], the frequency characteristics of the WPT system is studied, and a method to automatically tune the operating frequency to maintain optimum efficiency is proposed. Phase-locked loop techniques are able to tune the operating frequency to track the resonant frequency that will change due to the variation of gap length, misalignment, and tolerance variation of the tuning components [17]. Impedance

\[ U_{ab,mth} \] Phasor of the \( m \)-th order output voltage before rectifier.

\[ I_{L1,1} \] Phasor of the current on the primary-side compensation inductor \( L_{f1} \).

\[ I_1 \] Phasor of the current on the transmitting coil.

\[ I_2 \] Phasor of the current on the receiving coil.

\[ I'_2 \] Phasor of the current on the receiving coil referred to the primary side.

\[ I_{L2,1} \] Phasor of the current on the secondary-side compensation inductor \( L_{f2} \).

\[ I'_2 \] Phasor of the current on \( L_{f2} \) referred to the primary side.

\[ I_{L1,1AB} \] Phasor of the current on \( L_{f1} \) when only \( U_{AB} \) is applied.

\[ I_{1AB} \] Phasor of the current on the transmitting coil when only \( U_{AB} \) is applied.

\[ I_{2AB} \] Phasor of the current on the receiving coil when \( U_{AB} \) applied only referred to the primary side.

\[ I'_2 \] Phasor of the current on \( L_{f2} \) when \( U_{AB} \) applied only referred to the primary side.

\[ I_{1ab} \] Phasor of the current on the transmitting coil when only \( U_{ab} \) is applied.

\[ I'_2 \] Phasor of the current on the receiving coil when only \( U_{ab} \) is applied.

\[ I'_2 \] Phasor of the current on \( L_{f2} \) when \( U_{ab} \) applied only referred to the primary side.

\[ I_{L1,mth} \] Phasor of the \( m \)-th order current on \( L_{f1} \).

\[ I_{L1,1AB,1st} \] Phasor of the first-order current on \( L_{f1} \) when only \( U_{ab} \) is applied.

\[ I_{L2,mth} \] The phasor of the \( m \)-th order current on \( L_{f2} \).

\[ I_{OFF} \] Turn-off current of the MOSFETs.

\[ I_{OFF,\min} \] Minimum turn-off current of the MOSFETs.

\[ \varphi \] Phase by which \( U_{ab} \) leads \( U_{AB} \).

\[ \varphi_1 \] Phase by which \( I_{L2,1st} \) leads \( U_{AB} \).

\[ \varphi_2 \] Phase by which \( U_{ab} \) leads \( I_{L2,1st} \).

\[ U_{in} \] The dc input voltage.

\[ U_b \] Battery voltage.

I. INTRODUCTION

WIRELESS power transfer (WPT) using magnetic resonant concept was proposed by Nikola Tesla more than 100 years ago. Until recently, with the development of power electronics technology, it is realized that a WPT system can be implemented economically enough to have a commercial value. Several companies, such as WiTricity, Evatran, Qualcomm, etc., have already developed a few products that can transfer power with acceptable power level and efficiency through a certain air gap. A lot of new research, such as the amazing 2-m 60-W power transfer [1], various analysis and control methods [2]–[5], and the guided power transfer path using the domino-repeaters [6], [7], have also been published lately.

In a WPT system, the energy is transferred through the mutual inductance of the transmitting and receiving coils, whereas the leakage inductance does not have a direct contribution to the active power transfer. Because of the large gap between the transmitting and receiving coils, the coupling coefficient between the two coils is small, i.e., typically in the range of 5%–30% depending on the distance, alignment, and size of the coils. This causes the WPT systems to have a large leakage inductance but a small mutual inductance. To increase the coupling, the coil design, without a doubt, is important [8]. Meanwhile, the compensation circuit, which is used to cancel the leakage inductance, is also of great importance. Usually, capacitors, which can be lumped or parasitic, are added to form a resonant circuit, which is known as the magnetic resonant method.

Different compensation topologies have been proposed and implemented to tune the two coils working at a resonant frequency in a wide range of applications. There are four basic topologies depending on how the compensation capacitors are added to the transmitting and receiving coils, namely, series-series (SS), series-parallel, parallel-series, and parallel-parallel topologies [9], [10]. Some other novel topologies have also been proposed in the literature. In [11], a dual topology is realized by switching between a parallel-compensated secondary side and a series-compensated secondary side to realize both constant current mode and constant voltage mode. Moreover, the transmitting and receiving coils need to be connected to the power electronics converters. To achieve high efficiency for the complete WPT system, some other superior topologies have been proposed. In [12], an LCL converter is formed by adding LC compensation network between the converter and the transmitting coil. There are two advantages for the LCL converter when the system works at the resonant frequency. First, the inverter only supplies the active power required by the load; second, the current in the primary-side coil is independent of the load condition. In [13], an LC compensation network at both primary and secondary sides is proposed for bidirectional power transfer. The design of an LCL converter usually requires the same value for the two inductors. To reduce the additional inductor size and cost, usually, a capacitor is put in series with the primary-side coil, which forms an LCC compensation network. By utilizing an LCC compensation network, a zero current switching (ZCS) condition could be achieved by tuning the compensation network parameters [14]. Moreover, when the LCC compensation network is adopted at the secondary side, the reactive power at the secondary side could be compensated to form a unit power factor pickup [15].

One of the uniqueness of WPT systems is the high spatial freedom of the coils. This means the air-gap variation and misalignment of the transmitting and receiving coils are inevitable. Usually, the system parameters and resonant frequency of the primary and secondary resonant tanks change when the coupling condition changes [16]. With traditional compensation topologies, to achieve high efficiency, a tuning method is needed to maintain the resonance when the air gap changes or misalignment happens. There are two main methods, namely, frequency control [17], [18] and impedance matching [19], [20]. In [18], the frequency characteristics of the WPT system is studied, and a method to automatically tune the operating frequency to maintain optimum efficiency is proposed. Phase-locked loop techniques are able to tune the operating frequency to track the resonant frequency that will change due to the variation of gap length, misalignment, and tolerance variation of the tuning components [17]. Impedance
matching is adopted in [20]. A tuning circuit was added in the SS structure to increase the efficiency by changing the resonant frequency to match the operating frequency. Similarly, an automated impedance matching system was designed in [19], and in [21], two ways for tuning the primary tank are introduced: the primary capacitance and inductance. For the SS structure, when the capacitor is tuned with the coil self-inductance, a fully resonant characteristic can be realized [10], [22]. In this case, the resonant frequency is independent with the load and coupling condition. However, for SS compensation, the primary coil current varies with the coupling coefficient and load condition. There are a few benefits to have a constant primary coil current. When a coil is designed, the rated current of the coil is determined. A constant current feature can make the coil work at its rated condition easily. For a track form coil at the primary side in dynamic roadway charging, multiple receiving coils could be powered, which also prefers a constant current in the track. Moreover, the power is related to the primary-coil current, coupling, and load condition. When the coil current is not a function of coupling and load, the control of power can be simplified. To keep a constant primary-coil current, additional phase shift or duty cycle control is usually adopted to regulate the coil current, which increases the control complexity, circulating energy in the inverter, and the risk of losing soft switching condition.

The compensation network and the corresponding control method are the most important and difficult aspects in the design of a wireless charging system. In this paper, the compensation network design is focused. A double-sided LCC compensation topology and its parameter design are proposed. The topology consists of one inductor and two capacitors at both the primary and secondary sides. With the proposed method, the resonant frequency of the compensated coils is independent of the coupling coefficient and the load condition. The WPT system can work at a constant frequency, which eases the control and narrows the occupation of frequency bandwidth. Nearly unit power factors can be achieved for both the primary-side and secondary-side converters in the whole range of coupling and load conditions; thus, high efficiency for the overall WPT system is easily achieved. A parameter tuning method is also proposed and analyzed to achieve ZVS operation for the MOSFET-based inverter. The proposed method is more attractive in an environment where the coupling coefficient keeps changing, such as the electric vehicle charging application. Moreover, due to its symmetrical structure, the proposed method can be used in a bidirectional WPT system. Simulation and experimental results verified analysis and validity of the proposed compensation network and the tuning method. A prototype with output power of 7.7 kW for electric vehicles was built, and 96% efficiency from dc power source to battery load was achieved.

The double-sided LCC compensation network, as well as a theoretical analysis, is presented in Section II. The tuning method for realizing ZVS is discussed in Section III. The design method for the proposed topology is introduced in Section IV. Experimental, simulation, and theoretical results are compared in Section V. The conclusions are summarized in Section VI.

II. PROPOSED TOPOLOGY AND ANALYSIS

The proposed double-sided LCC compensation network and corresponding power electronics circuit components are shown in Fig. 1. $S_1 \sim S_4$ are four power MOSFETs in the primary side. $D_1 \sim D_4$ are the secondary-side rectifier diodes. $L_1$ and $L_2$ are the self-inductances of the transmitting and receiving coils, respectively. $L_f1$ and $C_f1$ and $C_1$ are the primary-side compensation inductor and capacitors, respectively. $L_f2$ and $C_f2$ and $C_2$ are the secondary-side compensation components, respectively. $M$ is the mutual inductance between the two coils. Here, $u_{AB}$ is the input voltage applied on the compensated coil, and $u_{ab}$ is the output voltage before the rectifier diodes. $i_1$, $i_2$, $i_{f1}$, and $i_{f2}$ are the currents on $L_1$, $L_2$, $L_{f1}$, and $L_{f2}$, respectively. In the following analysis, $U_{AB}$, $U_{ab}$, $I_1$, $I_2$, $I_{L_{f1}}$, and $I_{L_{f2}}$ are adopted to represent the phasor form of the corresponding variables.

For the first step, a concise characteristic of the proposed compensation network will be given by analyzing the first-order harmonics of the square voltage waveform at the switching frequency. The resistance on all the inductors and capacitors are neglected for simplicity of analysis. The accuracy of the approximations will be verified by circuit simulation and experiments in the latter sections. The equivalent circuit of the circuit in Fig. 1 referred to the primary side is derived as shown in Fig. 2. The apostrophe symbols indicate the variables of the secondary side referred to the primary side. We define the turns ratio of the secondary to primary side as

$$ n = \sqrt{\frac{L_2}{L_1}}. $$

Fig. 1. Double-sided LCC compensation topology for WPT.
The variables in Fig. 2 can be expressed by the following:

\[ L_m = k \cdot L_1 \]
\[ L_{s1} = (1 - k) \cdot L_1 \]
\[ L_{s2} = (1 - k) \cdot L_2 / n^2 \]
\[ L'_{f2} = \frac{L_{f2}}{n^2} \]
\[ C'_2 = n^2 \cdot C_2 \]
\[ C'_{f2} = n^2 \cdot C_{f2} \]
\[ U'_{ab} = \frac{U_{ab}}{n} \]

(2)

where \( L_m \) is the magnetizing inductance referred to the primary side. The apostrophe symbols, which also appear in the equations after, mean the converted values that refer to the primary side.

For a high-order system in Fig. 1, there are multiple resonant frequencies. In this paper, we do not focus on the overall frequency-domain characteristics. Only one frequency point, which could be tuned to a constant resonant frequency, is considered. In this paper, we do not focus on the overall frequency-domain characteristics. Only one frequency point, which could be tuned to a constant resonant frequency, is considered. The analysis is similar to that when \( U_{AB} \) is applied. However, for a high-order system, there are multiple resonant frequencies. In this paper, we do not focus on the overall frequency-domain characteristics. Only one frequency point, which could be tuned to a constant resonant frequency, is considered. The analysis is similar to that when \( U_{AB} \) is applied.

The solutions are

\[ L_{e1} = \frac{1}{j\omega_0} \left( \frac{1}{j\omega_0 C_1} + j\omega_0 L_{s1} \right) = L_{f1} - k \cdot L_1 \]  
\[ (4) \]
\[ L_{e2}' = \frac{1}{j\omega_0} \left( \frac{1}{j\omega_0 C_2'} + j\omega_0 L_{s2}' \right) = L_{f2}' - k \cdot L_1 . \]  
\[ (5) \]

(4) \]
\[ L_{e2}' = \frac{1}{j\omega_0} \left( \frac{1}{j\omega_0 C_2'} + j\omega_0 L_{s2}' \right) = L_{f2}' - k \cdot L_1 . \]  
\[ (5) \]

(5) \]

It forms another parallel resonant circuit with the voltage on \( C_{f2} \) equal to \( U_{AB} \), and the voltage on \( C_{f2} \) equals the voltage on \( L_m \). \( I_{1AB} \) and \( I'_{L2AB} \) can be easily solved, i.e.,

\[ I_{1AB} = \frac{U_{AB}}{j\omega_0 L_{f1}} \]  
\[ (7) \]
\[ I'_{L2AB} = \frac{kU_{AB} L_1}{j\omega_0 L_{f1} L_{f2}}. \]  
\[ (8) \]

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\[ I'_{L2AB} = \frac{kU_{AB} L_1}{j\omega_0 L_{f1} L_{f2}}. \]  
\[ (8) \]

When \( U'_{ab} \) is applied, the analysis is similar to that when \( U_{AB} \) is applied. An additional subscript \( ab \) is added to indicate that the current is contributed by \( U_{ab} \). The additional subscript \( AB \) indicates that current is contributed by \( U_{AB} \). To make the analysis clear, the series-connected capaci-

tor and inductor branches, i.e., \( C_1 \) and \( L_{s1} \) and \( C_{f2} \) and \( L_{s2}' \), are expressed using equivalent inductances \( L_{e1} \) and \( L_{e2}' \), where

\[ L_{e1} = \frac{1}{j\omega_0} \left( \frac{1}{j\omega_0 C_1} + j\omega_0 L_{s1} \right) = L_{f1} - k \cdot L_1 \]  
\[ (4) \]
\[ L_{e2}' = \frac{1}{j\omega_0} \left( \frac{1}{j\omega_0 C_2'} + j\omega_0 L_{s2}' \right) = L_{f2}' - k \cdot L_1 . \]  
\[ (5) \]

(4) \]
\[ L_{e2}' = \frac{1}{j\omega_0} \left( \frac{1}{j\omega_0 C_2'} + j\omega_0 L_{s2}' \right) = L_{f2}' - k \cdot L_1 . \]  
\[ (5) \]

(5) \]

It forms another parallel resonant circuit with the voltage on \( C_{f2} \) at the same resonant frequency \( \omega_0 \). Thus, \( I_{1AB} = 0 \). Because there is no current through \( L_{f1} \) and \( L_{f2}' \), the voltage on \( C_{f2} \) equals \( U_{AB} \), and the voltage on \( C_{f2} \) equals the voltage on \( L_m \). \( I_{1AB} \) and \( I'_{L2AB} \) can be easily solved, i.e.,

\[ I_{1AB} = \frac{U_{AB}}{j\omega_0 L_{f1}} \]  
\[ (7) \]
\[ I'_{L2AB} = \frac{kU_{AB} L_1}{j\omega_0 L_{f1} L_{f2}}. \]  
\[ (8) \]

(7) \]
\[ I'_{L2AB} = \frac{kU_{AB} L_1}{j\omega_0 L_{f1} L_{f2}}. \]  
\[ (8) \]
\[ U_{ab}' = \text{passive voltage generated according to the conduction mode of diodes } D_1 \sim D_4. \text{ It should be in phase with } I_{L2}. \text{ Since } I_{L2} = 0, U_{ab}' \text{ is in phase with } V_{L2}. \text{ If we take } U_{AB} \text{ as the reference, } U_{AB} \text{ and } U_{ab} \text{ can be expressed as} \]

\[ U_{AB} = U_{AB} \angle 0^\circ \]  
\[ U_{ab}' = \frac{U_{ab}}{j} = U_{ab}' \angle \varphi = U_{ab}' \angle -90^\circ \]

where \( \varphi \) is the phase by which \( U_{ab} \) leads \( U_{AB} \). From (11) and (12), we can see \( U_{ab}' \) lags \( U_{AB} \) by \( 90^\circ \). We substitute (2), (11) and (12) into (7)–(10) and sum up the current generated by \( U_{AB} \) and \( U_{ab}' \) to get

\[ I_{L_{f1}} = I_{L_{f1}} = \frac{kL_1U_{ab}'}{\omega_0L_{f1}L_{f2}} \angle 0^\circ  = \frac{k\sqrt{L_1L_2}U_{ab}}{\omega_0L_{f1}L_{f2}} \angle 0^\circ \]  
\[ I_1 = I_{1AB} = \frac{U_{AB}}{\omega_0L_{f1}} = \frac{U_{AB}}{\omega_0L_{f1}} \angle -90^\circ \]  
\[ I_2 = \frac{I_{L_{f2}}}{n} = \frac{I_{L_{f2}}}{U_{ab}' \angle 0^\circ} = \frac{U_{ab}'}{\omega_0L_{f1}L_{f2}} \angle 0^\circ \]  
\[ I_{L_{f2}} = \frac{I_{L_{f2}}}{n} = \frac{kL_1L_2U_{AB}}{\omega_0L_{f1}L_{f2}} \angle -90^\circ. \]  

From (11) and (13), we can see that the input voltage and current are in phase. The unit power factor for the converter is achieved, regardless of the coupling coefficient and battery voltage. Thus, resonant condition could be achieved, regardless of the coupling and load condition. The transferred power can be calculated by

\[ P = U_{AB} \cdot I_{L_{f1}} = \frac{\sqrt{L_1L_2}}{\omega_0L_{f1}L_{f2}} \cdot kU_{AB}U_{ab}'. \]

It can be seen that the output power is proportional to the coupling coefficient \( k \), input voltage \( U_{AB} \), and output voltage \( U_{ab}' \). Thus, a buck or boost converter can be inserted into either before the primary-side inverter or after the secondary-side rectifier to control the output power. For some applications, such as opportunity charging or dynamic charging for electric vehicles, an accurate continuous power is not necessary. In this case, the charging power can be controlled by switching the system between the maximum and zero output power. Thus, the buck or boost converter can be omitted.

III. PARAMETER TUNING FOR ZERO VOLTAGE SWITCHING

If the coils and compensation network parameters are designed exactly according to the above rules, all the MOSFETs will be turned on and off at a ZCS condition. However, ZCS is not a perfect soft switching condition in converters containing MOSFETs and diodes. To minimize the switching loss, it is better that all switches are turned on and off at a zero voltage switching (ZVS) condition. The parasitic output capacitance of the MOSFET holds the voltage close to zero during the turn-off transition. Therefore, the turn-off switching loss is very small [23]. However, in the turn-on transition, ZVS operation is required to prevent both body diode reverse recovery and parasitic output capacitance from inducing switching loss. To realize ZVS for a MOSFET, the body diode should conduct before the MOSFET does. It is essential that the MOSFET needs to be turned on at a negative current. For a full-bridge converter, this means the input impedance of the resonant network should be inductive. In this case, the resonant current lags the resonant voltage that forms the ZVS operation condition for all MOSFETs.

In this paper, the ZVS operation condition refers to ensuring the turn-off current to be positive to realize ZVS turn on of another MOSFET in the same arm. There can be several ways to tune the system parameters to ensure that the MOSFETs turn off at a positive current. Here, one simple way is introduced and analyzed.

To achieve ZVS, we just slightly increase the value of \( L_{c2} \). As shown in Fig. 4, the change of \( L_{c2} \) is \( \Delta L_{c2} \). Moreover, the superposition method is used to analyze the tuned circuit. When \( U_{AB} \) is applied to the circuit, the equivalent circuit is the same as in Fig. 3(a), i.e., \( I_{L_{f1}AB} \) is zero. However, when \( U_{ab}' \) is applied, \( I_{L_{f2}ab} \) is not zero. We solve the circuit again with the variation of \( \Delta L_{c2} \). and the following equations can be derived:

\[ I_{L_{f2}ab,1st} = -j \cdot \frac{U_{ab}}{\omega_0L_2} \cdot \Delta L_{c2} \]  
\[ I_{L_{f2},1st} = I_{L_{f2}ab} + I_{L_{f2}ab,1st} = \frac{kU_{AB}L_1}{j\omega_0L_{f1}L_{f2}} \]  
\[ = \frac{U_{ab} \cdot (\cos \varphi + j \cdot \sin \varphi)}{\omega_0L_2} \cdot \Delta L_{c2} \]  
\[ \cdot \left( \frac{kU_{AB}L_1}{\omega_0L_{f1}L_{f2}} \right) \]  
\[ I_{L_{f2}1st} = \frac{I_{L_{f2},1st}}{n} = \frac{U_{ab} \cdot \sin \varphi \cdot \Delta L_{c2} - j \cdot kU_{AB}L_1}{\omega_0L_2} \cdot \Delta L_{c2} \]  
\[ \cdot \left( \frac{U_{ab} \cdot \cos \varphi \cdot \Delta L_{c2}}{\omega_0L_2} \right). \]  

In the given equations, the subscript 1st is used to indicate that it is the first harmonic component of the corresponding item.
The phase of $U_{ab}$ is $\varphi$. Equation (12) shows that $\varphi$ is $-90^\circ$ when $\Delta L_{e2}$ is zero. When we increase $L_{e2}$ to realize ZVS, the change of $L_{e2}$ is relatively small; therefore, $\varphi$ is still close to $-90^\circ$. We have $\sin \varphi \approx -1$, $\cos \varphi \approx 0$, and $\Delta L_{e2} < L_{f2}$. Usually, the additional inductors $L_{f1}$ and $L_{f2}$, which are used as a reactive power compensator, are designed such that they are much smaller than the main coils. The following approximation can be obtained from (20):

$$\cos \varphi_1 \approx -\cot \varphi_1 \approx -\frac{U_{ab}}{U_{AB}} \cdot \frac{\Delta L_{e2} \cdot L_{f1}}{L_{f2} \cdot k \sqrt{L_1 L_2}}$$  \hspace{1cm} (21)

where $\varphi_1$ ($-90^\circ < \varphi_1 < -180^\circ$) is the phase by which $I_{Lf2\_1st}$ leads $U_{AB}$.

To reduce the switching loss, we prefer to achieve ZVS condition at a minimum turn-off current. This means that, at the switching point, the current is close to zero. The current slew rate at the switching point is high. A small phase error in the analysis will bring relatively large current error. If the phase error falls into the inductive region, it means a higher turn-off current and higher switching loss. If the phase error is close to the inductive region, it means a higher turn-off current.

The high-order harmonics of the square voltage should be considered. To reduce the switching loss and electromagnetic interference (EMI) problem. Therefore, the analysis accuracy of the turn-off current is very important. The high-order harmonics of the square voltage should be considered. The inductor–capacitor network from the primary side to the secondary side is a high-order filter. The high-order harmonics, the interaction between the primary and secondary sides can be neglected. Thus, the high-order current on $L_{f2}$ can be roughly calculated by

$$I_{Lf2\_3rd} \approx -\frac{U_{ab\_3rd}}{j \cdot 3 \omega_0 L_{f2}} = \frac{j 3 U_{ab\_3rd}}{8 \omega_0 L_{f2}}$$

$$I_{Lf2\_5th} \approx -\frac{U_{ab\_5th}}{j \cdot 5 \omega_0 L_{f2}} = \frac{j 5 U_{ab\_5th}}{24 \omega_0 L_{f2}}$$

$$\ldots$$

$$I_{Lf2\_(2k+1)th} \approx -\frac{U_{ab\_(2k+1)th}}{j \cdot (2k+1) \omega_0 L_{f2}} = \frac{j (2k+1) U_{ab\_(2k+1)th}}{(2k+1)^2 - 1) \omega_0 L_{f2}}$$

$$\ldots$$  \hspace{1cm} (22)

According to (22), the phase difference between $U_{ab\_mth}$ and $I_{Lf2\_mth}$ is $90^\circ$. Therefore, when $U_{ab}$ jumps at the time that $i_{Lf2} = 0$, $i_{Lf2\_mth}$ reaches the peak. Moreover, the peak value can be calculated by

$$\max \left\{ \sum i_{Lf2\_mth} \right\} = \sqrt{2} \cdot \sum_{k=1}^{\infty} I_{Lf2\_(2k+1)th} \approx \sqrt{2} \cdot \frac{U_{ab}}{\omega_0 L_{f2}}$$

$$= \sqrt{2} \cdot \frac{U_{ab}}{\omega_0 L_{f2}}. \hspace{1cm} (23)$$

Fig. 5 shows the effect of the high-order harmonic currents. The sign of $u_{ab}$ is determined by $i_{Lf2}$, which is a composition of both the first- and high-order harmonic currents.

From (21) and (24), the following equation can be derived:

$$\frac{U_{ab}}{U_{AB}} \cdot \frac{L_{f1}}{L_{f2}} \cdot \frac{\Delta L_{e2}}{L_{f2} - \frac{1}{4} \omega_0 L_{f1}} = -\frac{k U_{ab} L_{f1}}{\omega_0 L_{f1} L_{f2}^2} \left( \frac{\Delta L_{e2}}{L_{f2} - \frac{1}{4} \omega_0 L_{f1}} \right)$$

$$= -\frac{k U_{ab} L_{f1}}{\omega_0 L_{f1} L_{f2}^2} \left( \frac{\Delta L_{e2}}{L_{f2} - \frac{1}{4} \omega_0 L_{f1}} \right)$$

$$= \frac{k U_{ab} L_{f1}}{\omega_0 L_{f1} L_{f2}^2} \left( \frac{\Delta L_{e2}}{L_{f2} - \frac{1}{4} \omega_0 L_{f1}} \right)$$

$$= \frac{k U_{ab} L_{f1}}{\omega_0 L_{f1} L_{f2}^2} \left( \frac{\Delta L_{e2}}{L_{f2} - \frac{1}{4} \omega_0 L_{f1}} \right). \hspace{1cm} (26)$$

From (26), we can see an additional reactive current item is introduced. This current will increase the MOSFET turn-off current to achieve ZVS. For the primary side, similar to the analysis of the secondary side for the high-order harmonics effect, the following equations can be obtained:

$$\max \left\{ \sum i_{Lf1\_mth} \right\} = \sqrt{2} \cdot \sum_{k=1}^{\infty} I_{Lf1\_(2k+1)th} \approx \sqrt{2} \cdot \frac{U_{ab}}{\omega_0 L_{f1}} \cdot \frac{1}{\omega_0 L_{f1}}$$

$$= \sqrt{2} \cdot \frac{U_{ab}}{\omega_0 L_{f1}} \cdot \frac{1}{\omega_0 L_{f1}}. \hspace{1cm} (27)$$
The MOSFET turn-off current is a composition of both the first-order and high-order harmonic currents. From (26) and (27), the MOSFET turn-off current can be calculated as

$$I_{OFF} = \sqrt{2} \left( \frac{U_{AB}^2}{\omega_0 L_{f2}} \left( \frac{\Delta L_{e2}}{L_{f2}^2} - \frac{1}{4} \right) + \frac{U_{AB}}{4\omega_0 L_{f1}} \right). \quad (28)$$

According to the MOSFET parameters, a minimum turn-off current to achieve ZVS can be determined [24]. Then, a suitable \(\Delta L_{e2}\) can be designed to ensure that there is enough turn-off current to achieve ZVS for the whole operation range. To ensure \(I_{OFF}\) is greater than a certain positive value, the following equation should be satisfied:

$$\frac{\Delta L_{e2}}{L_{f2}} \geq \frac{1}{4}. \quad (29)$$

According to (28) and (29), the lower the output voltage is, the smaller the turn-off current is. The minimal turn-off current can be derived as

$$I_{OFF \_min} = \sqrt{2} \cdot U_{ab \_min} \cdot \sqrt{\frac{\Delta L_{e2}}{L_{f1}^2} - \frac{1}{4} \cdot \frac{L_{f1}^2}{L_{f2}^2}}. \quad (30)$$

where \(U_{ab \_min}\) is the minimum rms value of the output voltage before rectifier.

The minimal turn-off current is reached when

$$U_{AB} = U_{ab \_min} \cdot \sqrt{4 \cdot \left( \frac{\Delta L_{e2}}{L_{f2}^2} - \frac{1}{4} \right) \cdot \frac{L_{f1}}{L_{f2}}}. \quad (31)$$

Once the minimum MOSFET turn-off current is obtained, \(\Delta L_{e2}\) can be calculated by

$$\Delta L_{e2} = \frac{1}{4} L_{f2} \cdot \frac{I_{OFF \_min}^2 \omega_0^2}{U_{ab \_min}^2} + L_{f1}^2 \frac{L_{f2}^2}{U_{AB}^2}. \quad (32)$$

When the parameters are tuned for ZVS, the change of active power transferred is very limited. The conclusion could be obtained by analyzing the change of \(I_{L_{f2 \_1st}}\) and the phase between output current and voltage. In (20), the first term has one relative small item, and its contribution to the amplitude is negligible. The last term is a product of two relative small items, which can also be neglected. Compared with (13), the amplitude of \(I_{L_{f2 \_1st}}\) is almost the same. From (24), we can see the phase between the output current and voltage has no relation with \(\Delta L_{e2}\). Thus, \(\Delta L_{e2}\) does not have an obvious impact on the active power transferred. However, if the harmonics are considered, the output power in (17) should be revised to

$$P = \frac{\sqrt{L_1 L_2}}{\omega_0 L_{f1} L_{f2}} \cdot k U_{AB} U_{ab} \cos \varphi_2 \quad (33)$$

where \(\cos \varphi_2\) can be calculated from (24). If \(U_{AB}\) is not too low, \(\cos \varphi_2\) will be close to 1. The output power could be calculated by both (17) and (33).

The decomposition of current harmonics adopted in this section is a refinement of a similar approach that was used in the analysis of a ZCS LCC-compensated resonant converter [14]. In the referenced paper, the battery load was considered an equivalent impedance, which is a kind of first harmonics approximation. Although the high-order harmonics is hardly transferred between the primary-side and secondary-side coils, it does affect the reactive power at the secondary side, which will change the primary-side turn-off current. Here, the current harmonics are considered at both the primary and secondary sides. The secondary-side phase difference between the voltage and current fundamental harmonic could be solved, which means that the reactive power of the battery load with a rectifier was solved. In this way, (28) gives a direct method to calculate the turn-off current by the input and output voltages instead of an equivalent impedance of the battery load, which could be used to optimize the parameters easily.

### IV. Parameters Design

In this section, an 8-kW WPT system is designed according to the above principle. A comparison between the simulation results and the analytical results will be given in the following section to verify the effectiveness of the above analysis.
The specifications of the wireless battery charger are listed in Table I. Since the ratio between the input voltage and the output voltage is around 1, the transmitting and receiving coils are designed to have to same size. Thus, from (3), we should design $L_{f1} = L_{f2}$. From Table I and (17), we can get
\[
L_{f1} = L_{f2} = \sqrt{\frac{k_{\text{max}}}{U_{AB}} \cdot \frac{U_{ab}}{\omega_0 P_{\text{max}}} \cdot \frac{\pi^2}{2} \cdot \frac{U_{\text{ab}}}{L_1}} = \sqrt{0.32 \times \frac{2\sqrt{2} \times 425 \times \frac{2\sqrt{2}}{\pi} \times 450}{2\pi \times 79 \times 10^3 \times 8 \times 10^3} \cdot 360 \times 10^{-6}} \ \text{H}
\]
\[
\approx 67 \ \mu\text{H.}
\]
(34)

The value of $C_{f1}$ and $C_{f2}$ can be calculated from (3) as follows:
\[
C_{f1} = C_{f2} = \frac{1}{\omega_0^2 L_{f1}} \approx 60.6 \ \text{nF.}
\]
(35)

$C_1$ and $C_2$ can also be calculated from (3) as follows:
\[
C_1 = C_2 = \frac{1}{\omega_0^2 (L_1 - L_{f1})} \approx 14 \ \text{nF.}
\]
(36)

Then, a variation of $\Delta L_{e2}$ should be designed to increase the turn-off current for MOSFETs to achieve ZVS. Once the minimum turn-off current for ZVS is obtained, $\Delta L_{e2}$ can be designed using (32). For different MOSFETs and dead-time settings, the minimum turn-off current is different. For a 8-kW system, usually, a MOSFET with 80-A continuous conduction capability can be adopted. Fairchild FCH041N60E N-Channel MOSFET was chosen as the main switches. The switches are rated at 600 V and 48 (75°C)–77 A (25°C). According to the parameters of the MOSFET, the calculated dead time is 600 ns.

To guarantee ZVS in this mode, the turn-off current must be large enough to discharge the junction capacitors within the dead-time, which can be represented as follows: [24]
\[
I_{\text{OFF}} \geq \frac{4C_{\text{oss}} U_{AB, \text{max}}}{t_d}
\]
(37)

where $U_{AB, \text{max}}$ is the maximum input voltage, $C_{\text{oss}}$ is the junction capacitance, and $t_d$ is the dead time. By using the MOSFET parameters, we can calculate the turn-off current that should be larger than 2 A to realize ZVS. Thus, we design the minimum turn-off current $I_{\text{OFF, min}}$ to be 3 A.

By substituting (34)–(36), and $I_{\text{OFF, min}}$ into (32), we can get
\[
\Delta L_{e2} = \frac{1}{4} L_{f2} + \frac{I_{\text{OFF, min}}^2 \cdot \omega_0^2 \cdot L_{f1} \cdot L_{f2}^2}{2 \cdot U_{\text{ab, min}}^2}
\]
\[
= \left( \frac{67}{4} + \frac{3^2 \cdot (2\pi \cdot 79 \times 10^3)^2 \cdot (67 \times 10^{-6})^2 \cdot 67}{2 \cdot \left( \frac{2\sqrt{2}}{\pi} \cdot 300 \right)^2} \right) \ \mu\text{H}
\]
\[
\approx 21 \ \mu\text{H.}
\]
(38)

The equivalent inductance $L_{e2}$ is determined by $C_2$ and leakage inductance $L_{e2}$. Because of $L_{e2}$ is related to the self-inductance and coupling, it is more complicated if we tune $L_{e2}$ to change the value of $L_{e1}$. It is easier to tune $C_2$ to change the value of $L_{e2}$. From (3), we know that
\[
\Delta L_{e2} = \frac{1}{\omega_0^2 C_2} - \frac{1}{\omega_0^2 (C_2 + \Delta C_2)}.
\]
(39)
Then, the variation of $C_2$ can be calculated:

$$\Delta C_2 = \frac{\omega_0^2 \cdot \Delta L_{c2} \cdot C_2^2}{1 - \omega_0^2 \cdot \Delta L_{c2} \cdot C_2} \approx 1.1 \text{nF}. \quad (40)$$

Thus, to achieve ZVS, the value of $C_2$ should be tuned such that it is 1.1 nF larger than the value calculated by (36). All the designed values for the compensation network are listed in Table II.

Since the system is a high-order circuit, there might be another resonant point near $\omega_0$ with a sharp changing of the system characteristics. This may significantly affect the performance in a real system because of the parameter variations. The frequency characteristics of the circuit shown in Fig. 2 were given to check whether there is a sharp changing resonant point around $\omega_0$. In the simulation, the value of $C_2$ was 14 nF to verify the analysis results in Section II. To show the load influence, a load resistor $R_{ac}$ is the equivalent resistance when the battery is charging, connected between $a'$ and $b'$ in Fig. 2. When the battery charging power was between 5% to 100% power, the range of $R_{ac}$ is roughly from 10 to 200 $\Omega$. The frequency characteristics of the input impedance were analyzed under the coupling coefficient from 0.18 to 0.32. Two typical bode diagrams were shown in Fig. 6 with different load conditions at coupling coefficient of 0.18 and 0.32. In Fig. 6, we can see that there is a constant resonant frequency at about 79 kHz. Moreover, there are some other resonant frequencies. The lowest and highest resonant points do not change when the load changes, whereas they do change with the coupling coefficient. It should be noticed that, around $\omega_0$, another resonant point may exist at certain conditions. However, the change from $\omega_0$ to the neighboring resonant point is quite smooth, which means there will be no sudden change when the working frequency has a little drift from $\omega_0$.

V. SIMULATION AND EXPERIMENT RESULTS

Both simulation and experiments are undertaken to verify the proposed double-sided LLC compensation network and its tuning method. The circuit parameters have been shown in Tables I and II. We define two kinds of misalignments, i.e., X-misalignment (door-to-door or right-to-left), and Y-misalignment (front-to-rear), as shown in Fig. 7. When parking a car, the X-misalignment is much harder for the driver to adjust. Therefore, we choose X-misalignments for the simulation and experiments. Various misalignments are reflected by the different coupling coefficients. In this section, three coupling coefficients, namely, $k = 0.18, 0.24, 0.32$, corresponding to $X = 310, 230$, and 0 mm, respectively, and three output voltages, $U_b = 300, 400$, and 450 V, are chosen as case studies. The switching frequency is fixed at 79 kHz for all the cases.

A. Simulation Results

A model was built in LTspice to simulate the performance of the proposed topology. The simulation results for different coupling coefficients, input voltages, and output voltages were obtained. Fig. 8 shows the comparison between simulated and calculated output power for various conditions. The output power varies linearly with the input voltages for different coupling coefficients and output voltages.

For high input voltage and high coupling coefficients, the simulation and theoretical analysis agree well with each other. However, for low input voltage and low coupling coefficients, the simulation does not agree well with the analytical results. This is because, at low input voltage and low coupling coefficient, the diodes at the secondary side do not conduct all the time between $t_n + n \cdot T/2$ and $t_n + (n + 1) \cdot T/2$, which is shown in Fig. 9. A similar situation can also be found in the comparison results of turn-off current, as shown in Fig. 10.
Fig. 10. Simulation and theoretical results of the MOSFETs turn-off current $I_{OFF}$. (a) $k = 0.32$. (b) $k = 0.24$. (c) $k = 0.18$.

![Diagram](image)

Fig. 11. Experiment setup. (a) Physical setup of the WPT system. (b) Capture of efficiency from power meter at output power of 7.7 kW.

![Diagram](image)

Fig. 12. Experimental and theoretical calculation results of the power levels for the wireless charger system. (a) $k = 0.32$. (b) $k = 0.24$. (c) $k = 0.18$.

B. Experimental Results

Fig. 11(a) shows the experimental setup. The coil dimension is 800 mm in length and 600 mm in width. The gap between the two coils is 200 mm. A 10-$\mu$F capacitor ($C_o$) and 10-$\mu$H inductor ($L_o$) are selected as the output filter. The coils are connected to the input inverter and output rectifier through an LCC compensation network. An electronic load at constant voltage mode was adopted to take the position of a real battery for easy voltage adjustment. Fig. 11(b) shows the efficiency screen shot from power meter Yokogawa WT1600 at output power of 7.7 kW. $U_{dc1}$ and $I_{dc1}$ are the input dc voltage and current, whereas $U_{dc2}$ and $I_{dc2}$ are the output dc voltage and current. $P_1$ and $P_2$ are the input and output power, and $\eta$ is the efficiency from dc power supply to the electronic load. $I_{ac2}$ is the output current ripple into the electronic load. Fig. 12 shows the comparison of experimental and simulation output power as a function of input voltage for three coupling coefficients and three output voltages. Different coupling coefficients are obtained by adjusting the gap and misalignment between transmitting and receiving coils. The output power matches well between simulation and experimental results, and they vary linearly with the input voltage. The same inconsistency
phenomenon happens at the low input voltage and low coupling conditions, as stated previously. The calculated and simulated maximum efficiency is 97.1%. Because of the resistance and parameter variations in the real system, the maximum efficiency of 96% was reached at output power of 7.7 kW, which is a little lower than the simulated result.

Fig. 13 shows the comparison of experimental and theoretical calculated turn-off currents of the MOSFETs. The experimental results agree well with the analytical results. Fig. 13 also verifies a good characteristic of the proposed tuning method. From (28), we can see the turn-off current is not a function of the coupling coefficient $k$. Once the parameters are designed and tuned, the ZVS condition could be achieved for all coupling conditions easily. The primary-side waveforms and secondary-side waveforms are shown in Fig. 14 when the system operates at steady state, delivering 7.2 kW to the load. At this operating point, input voltage $U_{in} = 400$ V, output voltage $U_b = 450$ V, coupling coefficient $k = 0.32$. The results indicate a good ZVS condition with $I_{OFF} = 5.6$ A. The turn-off current maintains higher than required, whereas it is quite small relative to the peak current.

Fig. 14. Waveforms of the input voltage $u_{AB}$ and current $i_{L1}$ and output voltage $u_{ab}$ and current $i_{L2}$ when delivering power of 7.2 kW. $U_{in} = 400$ V, and $U_b = 450$ V.

Fig. 15 shows the simulation and experimental efficiencies from dc power source to the battery load for the proposed double-sided LCC compensation network for WPT system. In the experiment, we use a constant voltage mode electronic load to represent the battery pack for flexible voltage adjustment. A power meter WT1600 from Yokogawa was connected in the system to calculate the efficiency by measuring the output power from dc source and the input power to the electronic load. From Fig. 15(c), we can find that the efficiency is very high even at a large X-misalignment condition. The maximum simulated efficiency is 97.1%, whereas the maximum measured efficiency is about 96% when $U_{in} = 425$ V, $U_b = 450$ V, and $k = 0.32$, as shown in Fig. 15(a). Table III gives a rough loss distribution at output power of 7.7 kW among different parts in the system. The large voltage and current dynamic range and the fast transient switching procedure make it hard to measure the loss of MOSFETs and diodes accurately. The loss of MOSFETs and diodes are estimated by spice-model-based simulation, whereas for the losses of all the other passive components, they were calculated by the current rms value and ac resistance from experiment. From Table III, we can see...
almost half of the loss was brought by the main coils, which means if we would like to increase the efficiency further, the optimization of the coils is still the most important approach.

VI. CONCLUSION

In this paper, a double-sided LCC compensation network and its tuning method have been proposed. The novel topology and tuning method ensure that the resonant frequency is independent of coupling coefficient and load conditions, and the ZVS condition for the MOSFETs is realized. The detailed mathematical analysis of the model was presented, as well as the design method. Simulation and experimental results validated the topology and tuning method. A 7.7-kW prototype was designed and built using the method proposed in this paper. The simulated system efficiency from dc power source to battery is 97.1%, and the measured efficiency is as high as 96%.

REFERENCES


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